

Swanson School of Engineering

JPCP Joint Design

WTS

PITT IRISE

ASHE Pittsburgb

2025 Transportation Forum

Presenter:

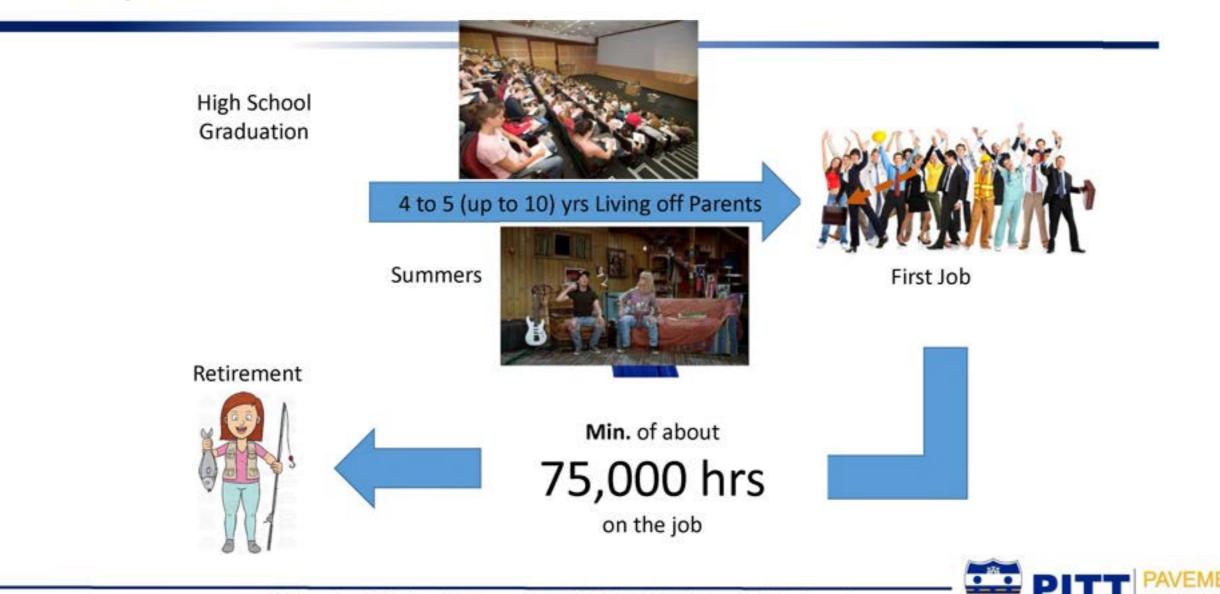
Julie Vandenbossche, PhD, PE Willman Kepler Whiteford Professor Associate Chair of Research IRISE, Director of Research

March 19, 2025



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The path we walk ...

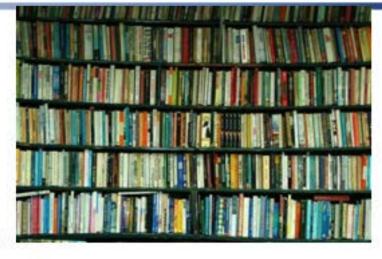




Defining Impact

Academic definition:

NUMBERS.... Number of publications Numbers of students Number of research dollars Number of committees served on Etc.....



Impact?

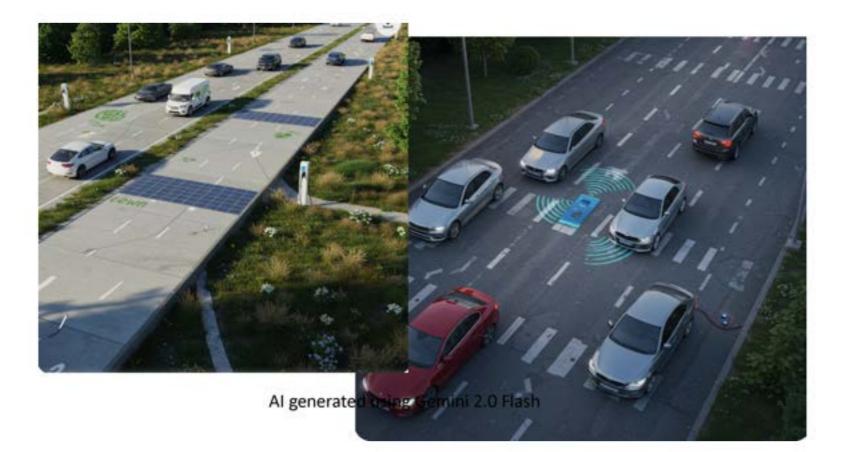




Quantifying true impact can be more of a challenge



Contribute to the transformation of research and ideas into practice....





Contribute to the transformation of research and ideas into practice....



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- Idea development
 Research
 Design
 - Design
 - Construction
 - Integration
 - ...



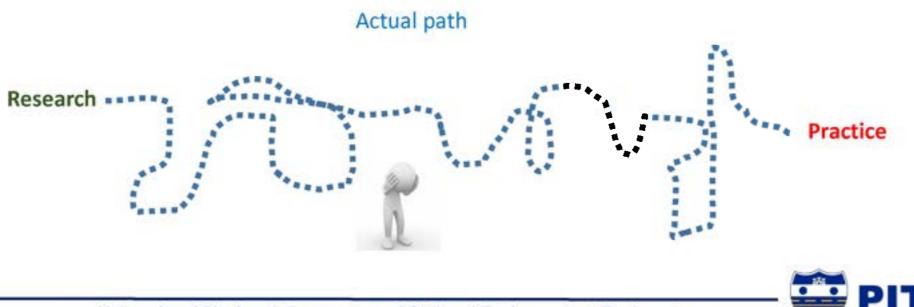


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Transforming research into practice

Research starts with a guess

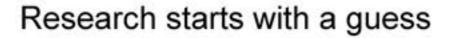




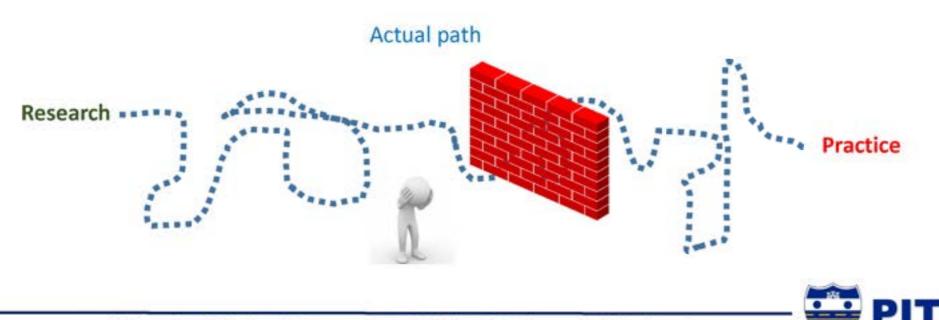


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Transforming research into practice









Transforming research into practice

Research starts with a guess







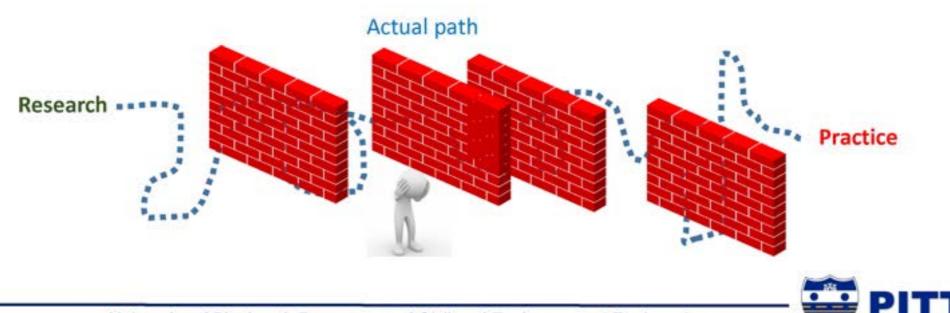


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Transforming research into practice

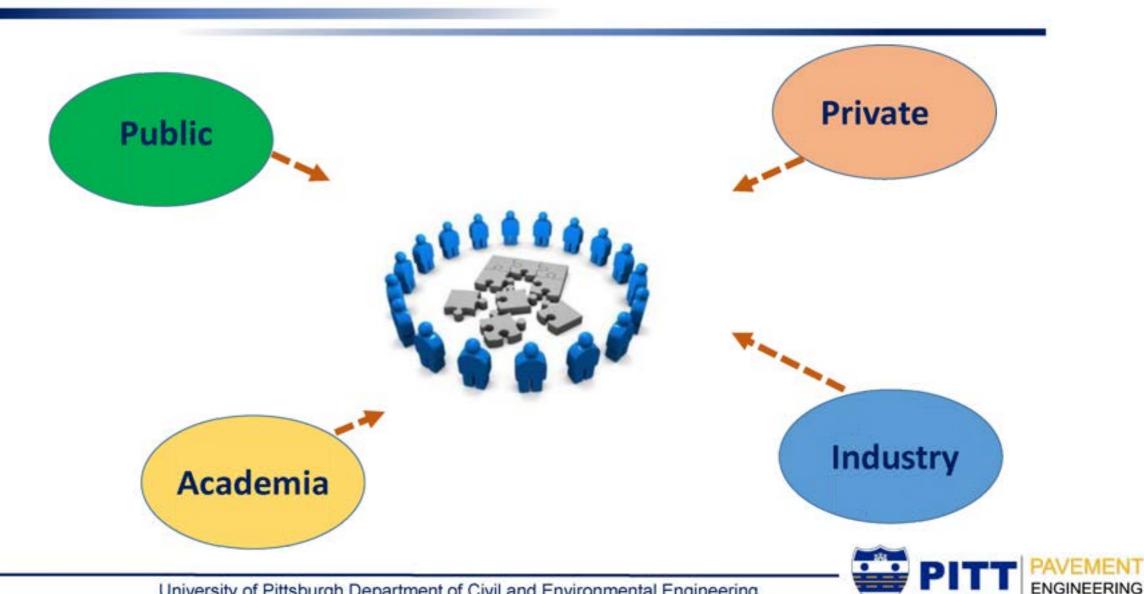
Research starts with a guess







Breaking through barriers...





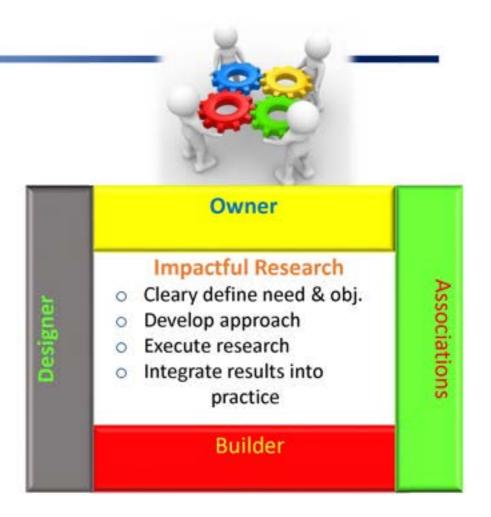
IRISE

Approach...

- o Get all parties involved early in the process
- Maintain their involvement throughout the process

Working together...

- Identify a deficiency/challenging issue
- Develop impactful technology
- Benefit seen by all parties (buy-in)



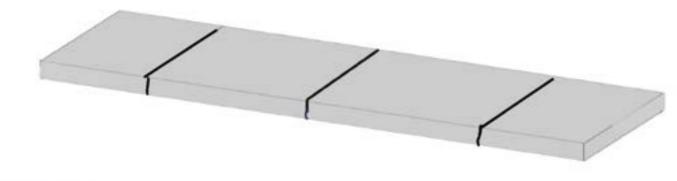




Slab design philosophy

- 1. Slab thickness => prevent fatigue cracking
- 2. Slab length (joint spacing) =>
 - a. Longer:
 - decrease costs associated with construction/maintenance of them
 - b. Too long:

- developing mid-slab cracking
- hinder jt. performance







JPCP Slab design philosophy

- 1. Slab thickness => prevent fatigue cracking (rarely occurs)
- 2. Slab length (joint spacing) =>
 - a. Longer:
 - decrease costs associated with construction/maintenance of them
 - b. Too long:
 - developing mid-slab cracking
 - hinder jt. performance

hinder jt performance

Longer slab => larger joint opening

- Lower agg interlock load transfer
- More difficult to keep sealed



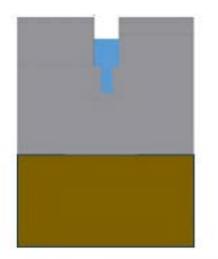


Joint performance - Concrete durability

- Durable concrete mixture PEM
- Concrete < 85% saturated (Taylor et al. in 2012)
 - · Avoid ponding in the joint
 - Well-sealed joint
 - Activated joints
 - Drainable base



Reduced potential for PCC distress



Increased potential for PCC distress





Joint performance - Design

1. Drainable base

(Erosion, pumping) 2. Effective load transfer

3. Joint sealing

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Reduced potential for pumping & erosion





Joint performance - Design

- 1. Drainable base
- 2. Effective load transfer

(Faulting, corner breaks)

3. Joint sealing

- a. Light truck traffic or short joint spacing:
 - aggregate interlock
- b. 20 to 30 yr- design life:
 - epoxy coated dowels
- c. Long-life pavement:
 - Long-life dowels (zinc galvanized, zinc clad, stainless steel, FRP)

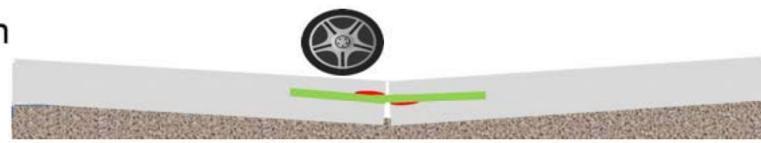


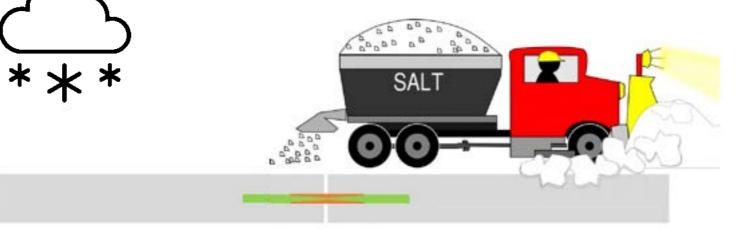


IRISE Dowel Corrosion

Goal: New faulting model that accounts for

- concrete damage based on
 - diameter
 - material stiffness
- dowel corrosion











Joint performance - Design

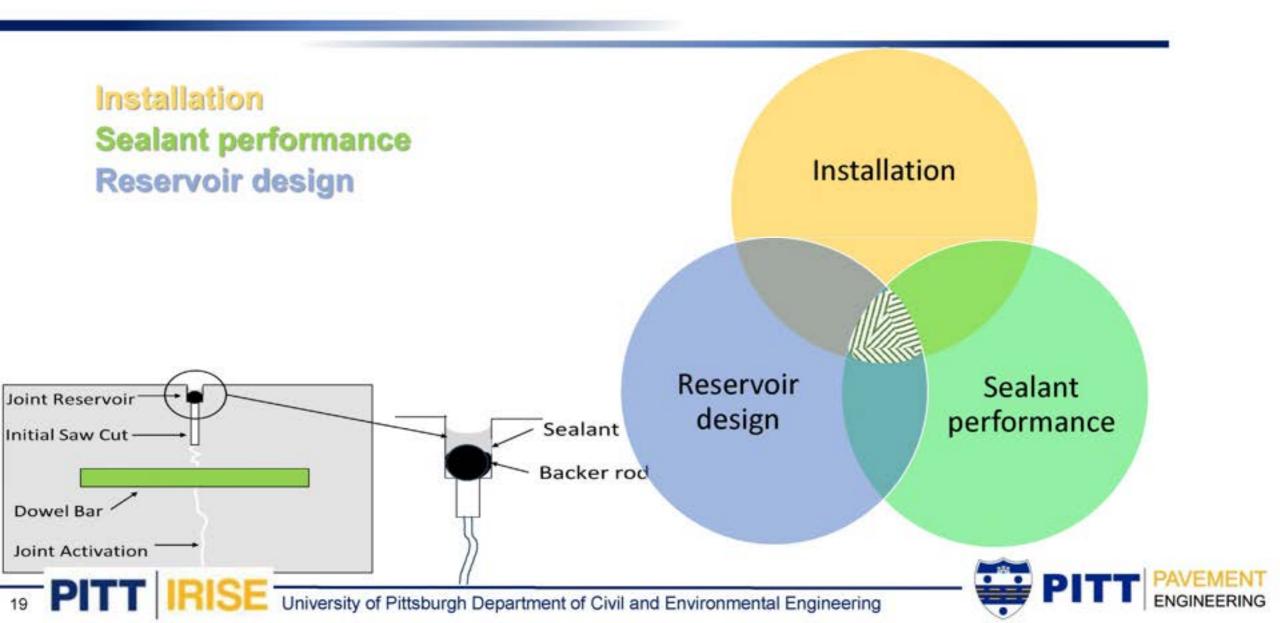
- 1. Drainable base
- 2. Effective load transfer
- 3. Joint sealing

- prevent entrance of deicing salts
 - (Dowel corrosion faulting, PCC durability)
- prevent entrance of water
 - (Pumping, erosion, dowel corrosion, PCC durability)
- prevent incompressibles (small pebbles and sand)
 - (Spalling, blowups)





Transverse Jt. sealant performance





Installation

Reservoir

design

Transverse Jt. sealant performance

Installation

- Wipe test (is this sufficient?)
- Wet saw vacuum

Sealant performance Reservoir design



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washing and vacuum

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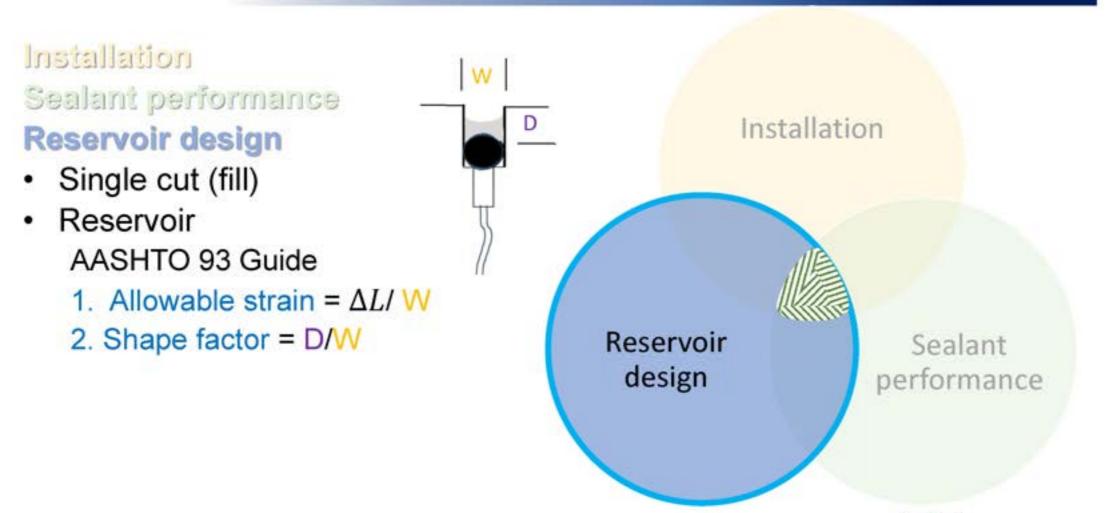


Sealant

performance



Task C: Transverse Jt. sealant performance



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Task C: Transverse Jt. sealant performance

Installation Sealant performance Reservoir design

- · Single cut (fill)
- Reservoir
 AASHTO 93 Guide
 - 1. Allowable strain = $\Delta L/W$ Cohessive failure
 - 2. Shape factor = D/W Adhesive failure







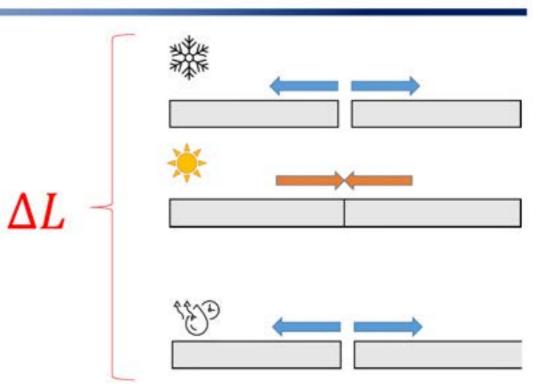
Task C: Transverse Jt. sealant performance

- Installation Sealant performance Reservoir design
- AASHTO 93 Guide

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- 1. Allowable strain = $\Delta L/W$
- 2. Shape factor = D/W





Allowable strain and Shape factor = f (sealant type)





Task C: Predicted reservoir resign width

 $\Delta L_{design(Old)} = CL(\Delta T\alpha + \varepsilon_{DS})$ $\Delta L_{design(New)} = L(C_{Therm}\Delta T\alpha + C_{D.S.}\varepsilon_{DS})$ Smart Pavement Data Where, L = 15 ft C_{therm} = 1 (Field value) ΔT = 85°F - 20°F = 65°F α = 5.71/°F (Lab value) C_{D.S.} = 0.20 (Field value) ε_{DS} = 630 με (Lab value) C = 0.65 (Old value) Therefore, • $\Delta L_{design} = 0.084$ in

ΔL_{design} = 0.114 in



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Field measured joint widths

Project	Pavement Construc. Year	Type of Sealant	Age of Pave. (Years)	Age of Sealant (Years)	Ave. Jt. Width (in)	Max. Jt. Width (in)	Min. Jt. Width (in)	Max. Jt. Opening (in)	Min. Jt. Opening (in)
A02N	2003	Type IV	18	2	0.50	0.63	0.43	0.25	0.06
A02S	2006	Type IV	15	2	0.42	0.51	0.35	0.14	-0.02
A05	2015	Type II	6	4	0.38	0.55	0.28	0.18	-0.10
A08A	2002	Type II	20	1	0.59	0.71	0.47	0.33	0.10
A10	2014	Silicone	8	8	0.54	0.59	0.43	0.21	0.06
A12A	2016	Type II	5	5	0.50	0.51	0.47	0.14	0.10
A12B	2018	Type IV	3	3	0.48	0.55	0.43	0.18	0.06

Theoretical $\Delta L @ 20F = 0.084$ in

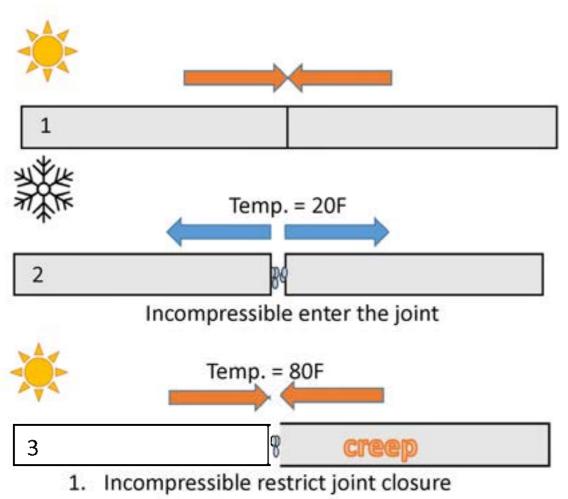
Thanks to Lydia Peddicord (PennDOT)

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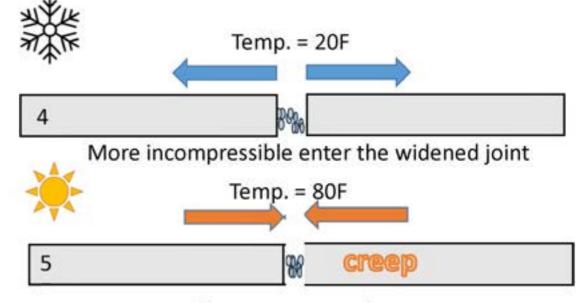




Sealant failure: joint widths can widen over time...



- 2. Stress builds up
- 3. Stress relaxation through creep so joint width at zeros stress increases



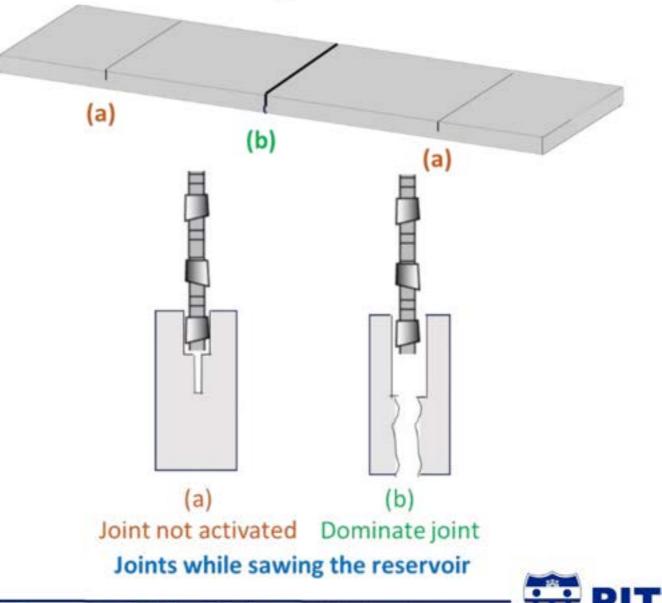
- 1. Incompressible restrict joint closure
- 2. Stress builds up
- Stress relaxation through creep so joint width at zeros stress increases again



Sealant failure: dominant joints



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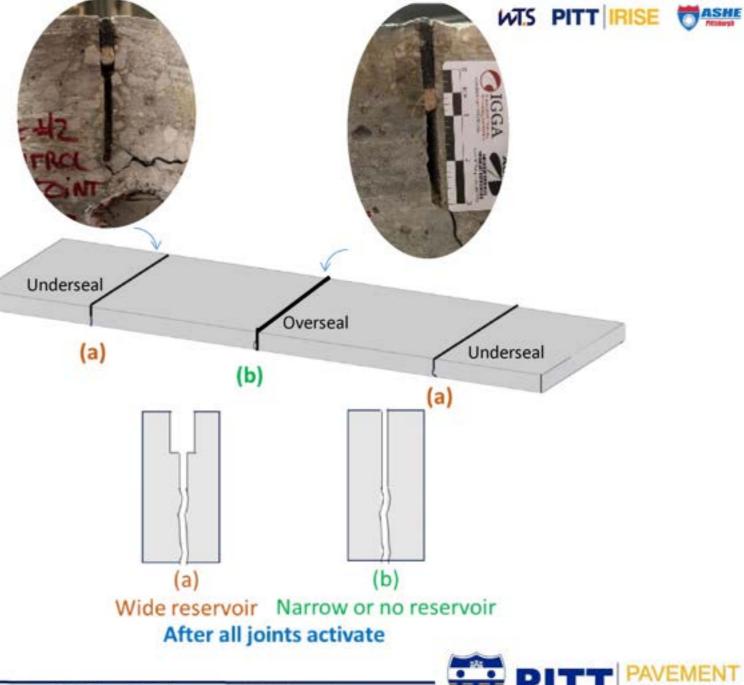


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Sealant failure: dominant joints

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Transverse Jt. sealant performance

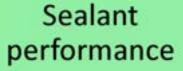
Installation

Sealant performance

- Silicone vs Type II and Type IV (Type IV still not performing as previous?)
 - ASTM D6690: Standard Spec. for Joint and Crack Sealants, Hot Applied, for Concrete and Asphalt Pavements
 - ASTM D5893: Standard Spec. for Cold-Applied, Single-Component, Chemically Curing Silicone Joint Sealant for Portland Cement Concrete Pavements

Reservoir design









Sealant materials

Sealant meets material specs/performance requirements

- Adhesion/cohesion requirements in ASTM 5329
- Closed-cell backer rod
- Fatigue exposure typically not considered



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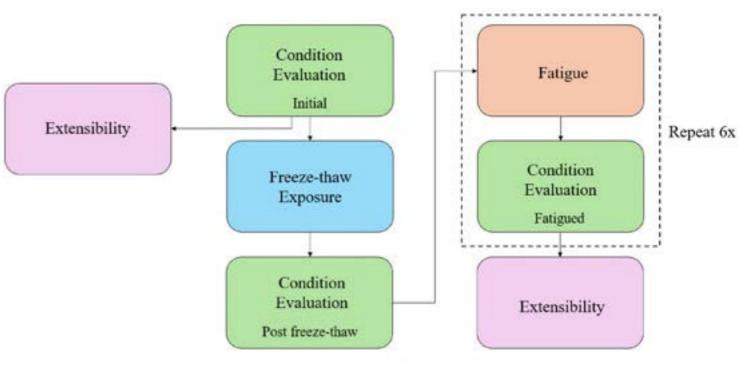
Objective 1: Characterize 42 yrs of simulated fatigue

Simulated field conditions:

- Exposure:
 - Freeze-thaw cycles
- Fatigue
 - Joint opening/closing (thermal loading)
 - Vertical (vehicle loading)

Condition assessment:

- Joint permeability
- Sealant stiffness



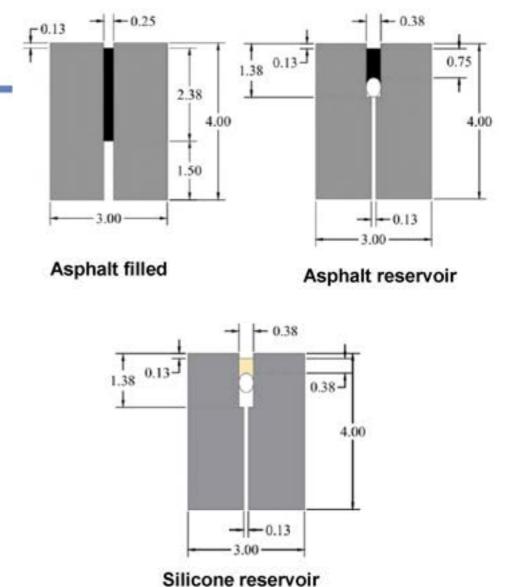




- Asphalt: P&T Products Dura-Fill 3405 LM (K)
- Silicone: Sikasil 728 Non-Sag Silicone Sealant
- · Asphalt filled
 - ACPA recommendation
 - Sealant W:D = 1:9.5
- Asphalt reservoir
 - Detail D Pub 72M
 - Sealant W:D = 1:2
- Silicone reservoir

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- Joint Type P Pub 72M
- Sealant W:D = 1:1

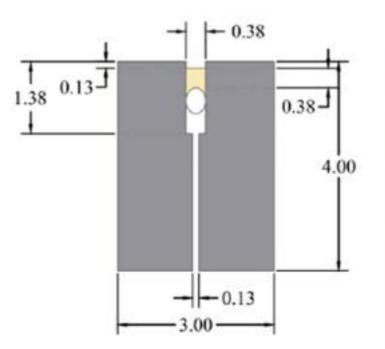


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Pavement CamoSeal by Main Street Materials

- Caltrans Approved (Recently)
- Joint Type P Pub. 72M
- Sealant W:D = 1:1









Pavement CamoSeal by Main Street Materials

- Poor performance in preliminary testing
- Joint opening/closing: immediate adhesive & cohesive failure
- Vehicle loading: immediate cohesive failure

Manufacturer suggested different blend better suited for colder climates









Pavement CamoSeal by Main Street Materials

- Poor performance in preli
- Joint opening/closing: i adhesive & cohesive f
- Vehicle loading: imme failure

Manufacturer suggest blend better suited for c climates

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Fatigue – Joint Opening/Closing

Initial protocol:

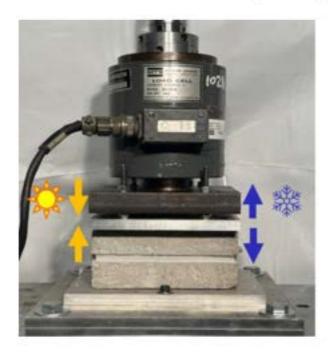
- Cycle between +53 and +78 mils (SR-22 TC data: ave. daily low -1 std dev ~ ave. daily high +1 std. dev.)
- 5,100 cycles (~42 yrs)

No damage accumulation under typical conditions

Revised protocol:

 Cycle between +53 and +186 mils (PennDOT joint sealant survey)

Joint opening Nov. - Feb. months



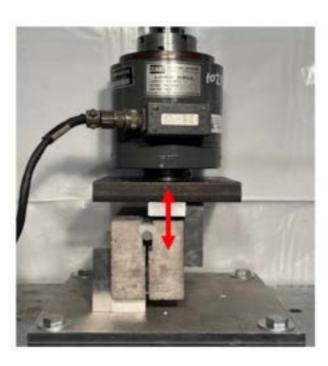
- Haversine wave @ 1 Hz
- Test temp. = 20°F



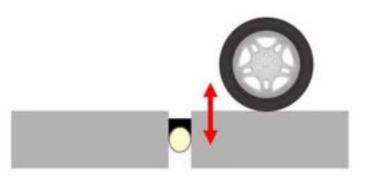


Fatigue – Vehicle loading

- Cycle +/- 10 mils
- 42 years (30,000 cycles @ 5 Hz
- Haversine wave
- Test temp. = 20°F



Vehicle loads







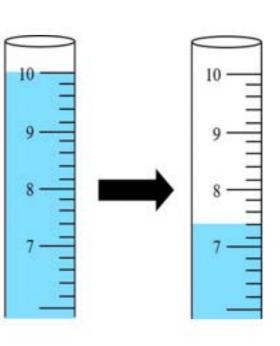
Condition Evaluation: joint permeability

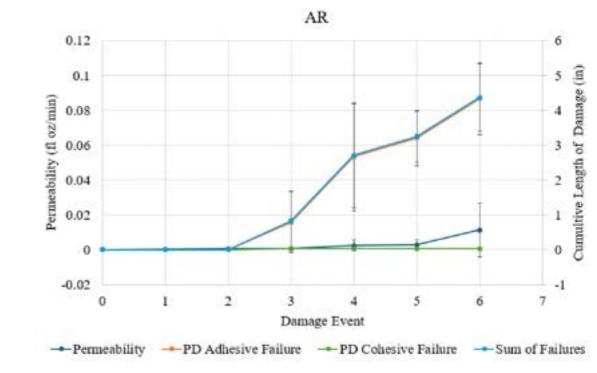
Permeability Apparatus



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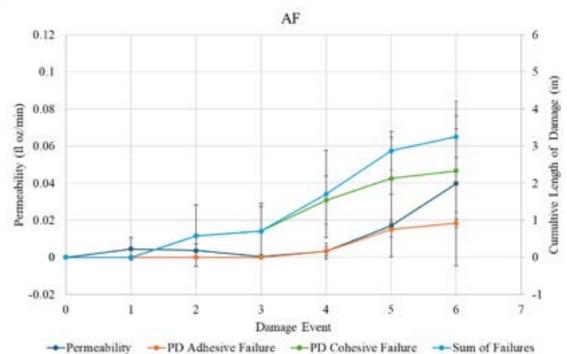






Findings: Permeability and damage accumulation

- Damage does not occur due to vehicle loading
- Asphalt filled
 - PD adhesive & cohesive damage
- Asphalt reservoir
 - PD adhesive damage
- Silicone reservoir
 - Minimal damage
 - · FD adhesive failure from poor seal
 - Minimal change in permeability



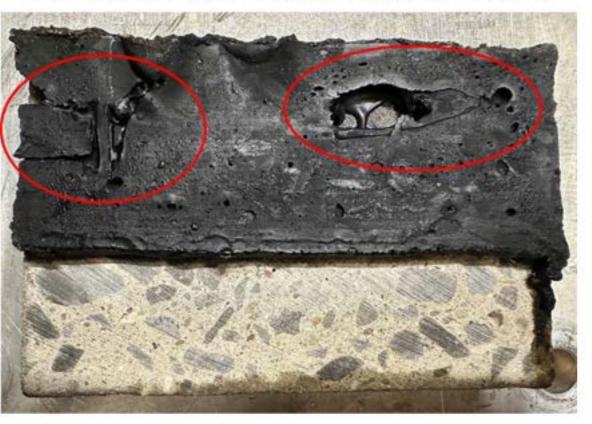




Findings: sealant stiffness

- Variability in asphalt filled joint performance
- · Difficult to fully fill narrow joint
- Voids/gaps in bulk sealant
- Lower apparent stiffness

Imperfections in sealant for asphalt filled joint







Findings: Extensibility

- Typical joint openings (0.04 to 0.07 in) sufficiently large to fail asphalt filled joint
- Performance better for silicone reservoir design than asphalt designs

Loss in performance from oxidation not considered

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Acknowledgements

- IRISE Consortium members
- · Edward Skorpinski (PA Turnpike Commission)
- James Young and Brandon Farrel (Gulisek)
- Lydia Peddicord (PennDOT)
- Tom Bryan (Bryan Concrete) and Justin Bryan (Neville Aggregates)
- Jack Parkhurst (University of Pittsburgh)
- Katey Doman (Tye Bar)





IRISE Funding



Denotes Founding Members

"Ex-Officio" Member





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Thank you

Questions?

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